

# Thermo-Mechanical Finite Element Simulation and Fatigue Life Assessment of a Copper Mould

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## ABSTRACT

This work describes the thermo-mechanical analysis of a copper mould for continuous steel casting. During the continuous casting process, the molten steel passes through a water cooled mould. The inner part of the component is subjected to a huge thermal flux. Consequently large temperature gradients occur across the mould, especially in the region near to the meniscus. As a result, considerable stresses and plastic strains are induced, which leads to deformations and thermal cracks at the inner surface. In order to assess the fatigue life of the copper mould, a three-dimensional finite element model is analyzed in dependence with different material models (combined nonlinear kinematic and nonlinear isotropic, linear kinematic, stabilized and accelerated material models). Material coefficients for adopted material models and fatigue curves are estimated from isothermal low cycle experimental fatigue data at different temperature levels (20 °C, 250 °C and 300 °C). The fatigue life is also assessed depending on different material models.

## Modelling

Hardening models - define evolution of the yield surface

### Isotropic hardening

#### Linear

Subsequent yield surface  
Initial yield surface  
 $R = R(\epsilon_{pl,acc})$

#### Nonlinear

Subsequent, expanded yield surface after plastic deformation  
Initial yield surface  
 $R = \sigma_0 + R_\infty [1 - \exp(-b\epsilon_{pl,acc})]$

### Kinematic hardening

#### Linear (Prager)

Subsequent yield surface  
Initial yield surface  
 $d\alpha = \frac{2}{3} C d\epsilon_{pl}$

#### Nonlinear (Armstrong & Frederick)

Subsequent yield surface  
Initial yield surface  
 $d\alpha = \frac{2}{3} C d\epsilon_{pl} - \gamma \alpha d\epsilon_{pl,acc}$

#### Nonlinear (Chaboche)

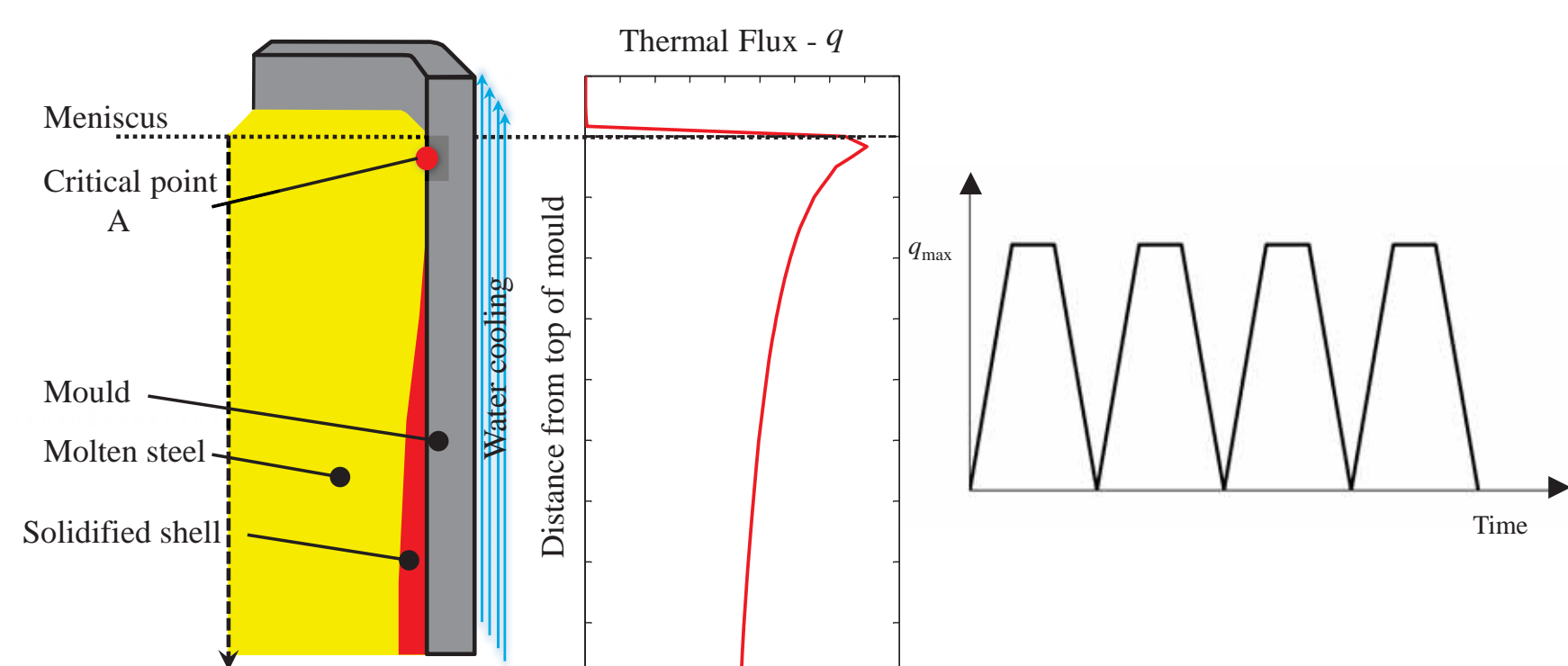
$\alpha = \sum_i \alpha_i$   $d\alpha_i = \frac{2}{3} C_i d\epsilon_{pl} - \gamma_i \alpha_i d\epsilon_{pl,acc}$

### Combined hardening (Nonlinear Iso. + Nonlinear Kin.)

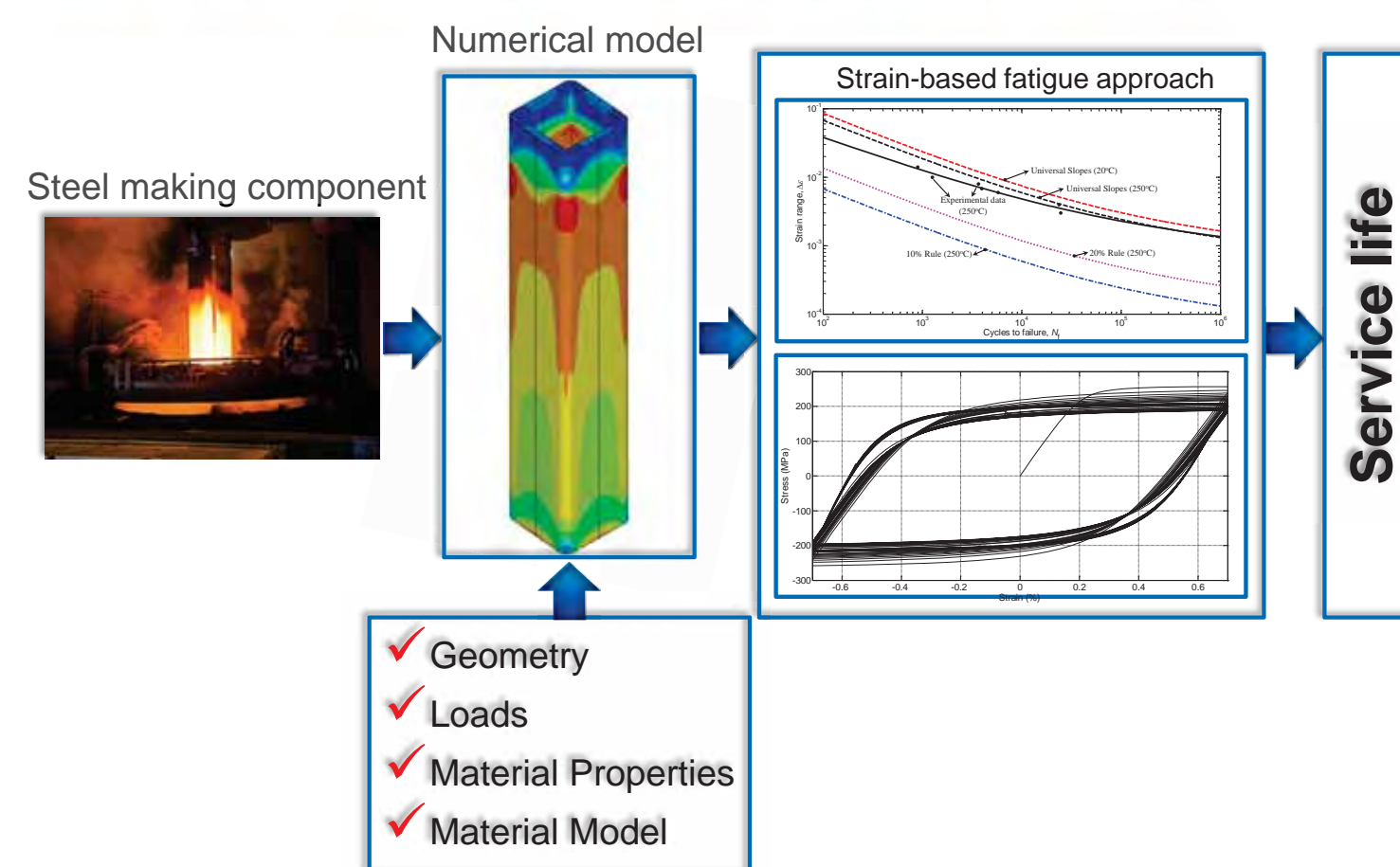
Limiting yield surface  
Current yield surface  
Limiting value of  $\alpha$

## Description of component

The molten steel flows from the upper part of the mould to the bottom part where the steel exits with a thin solidified shell. During the solidification of the steel, a huge thermal flux,  $q$ , passes from the molten steel to the inner surface of the mould, which is then subjected to high temperatures. The thermal flux varies according to a loading condition called macro cycle. Macro cycle is when the plant is switched on and the thermal flux increases until reaching the maximum value  $q_{max}$ , while thermal flux is absent once the plant is switched off.

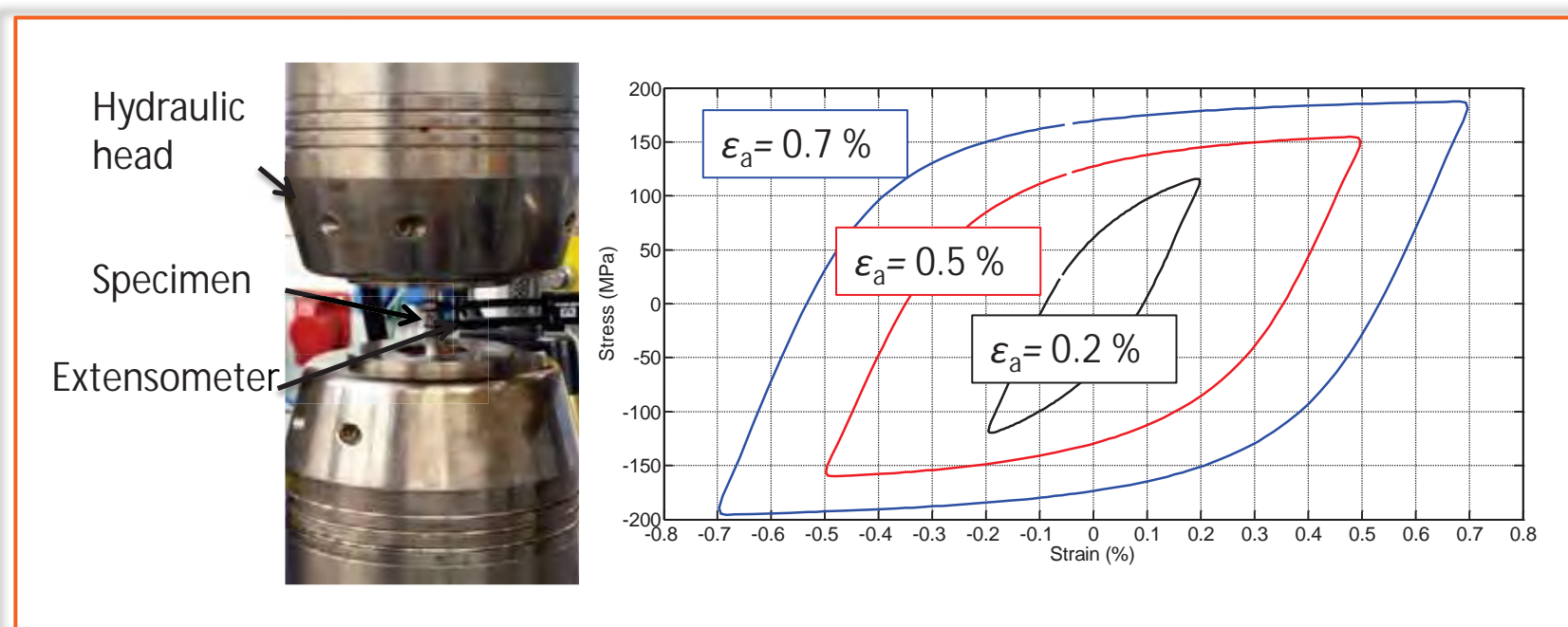


## Structural integrity and FEM

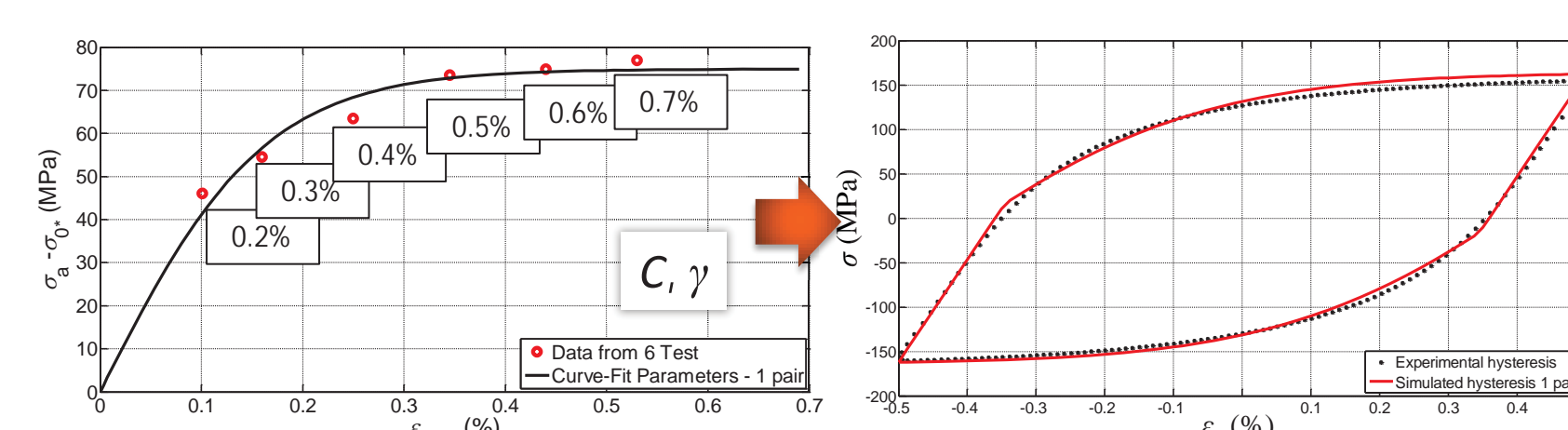


## Calibration of material models

Low cycle fatigue tests are performed for CuAg material at 20°C, 250°C and 300°C and at different strain amplitudes,  $\epsilon_a$ .



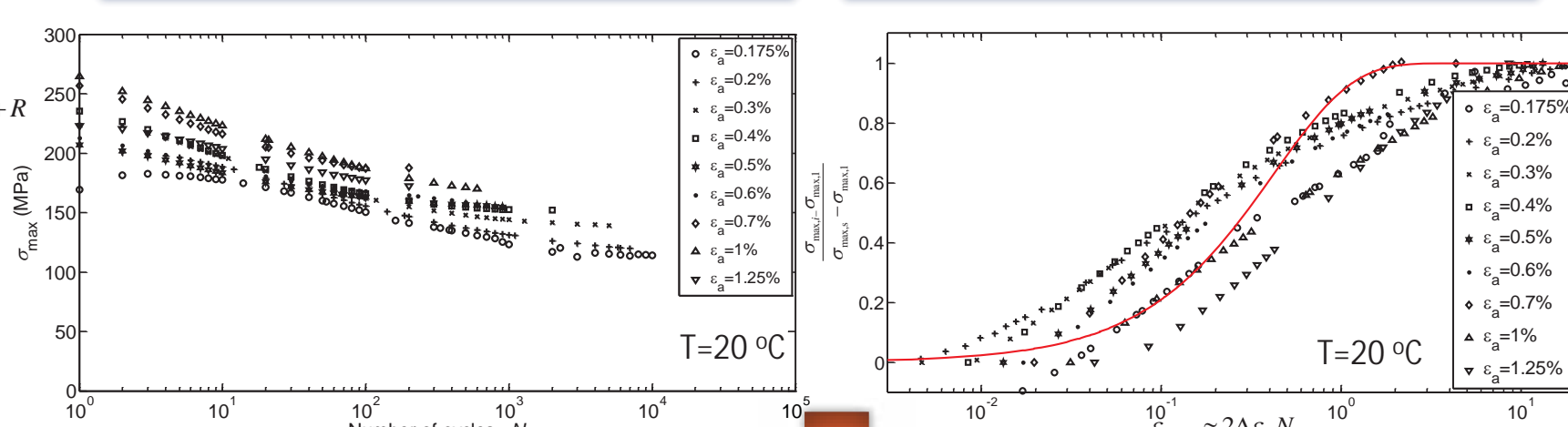
### 1) Parameters identification for nonlinear kinematic model



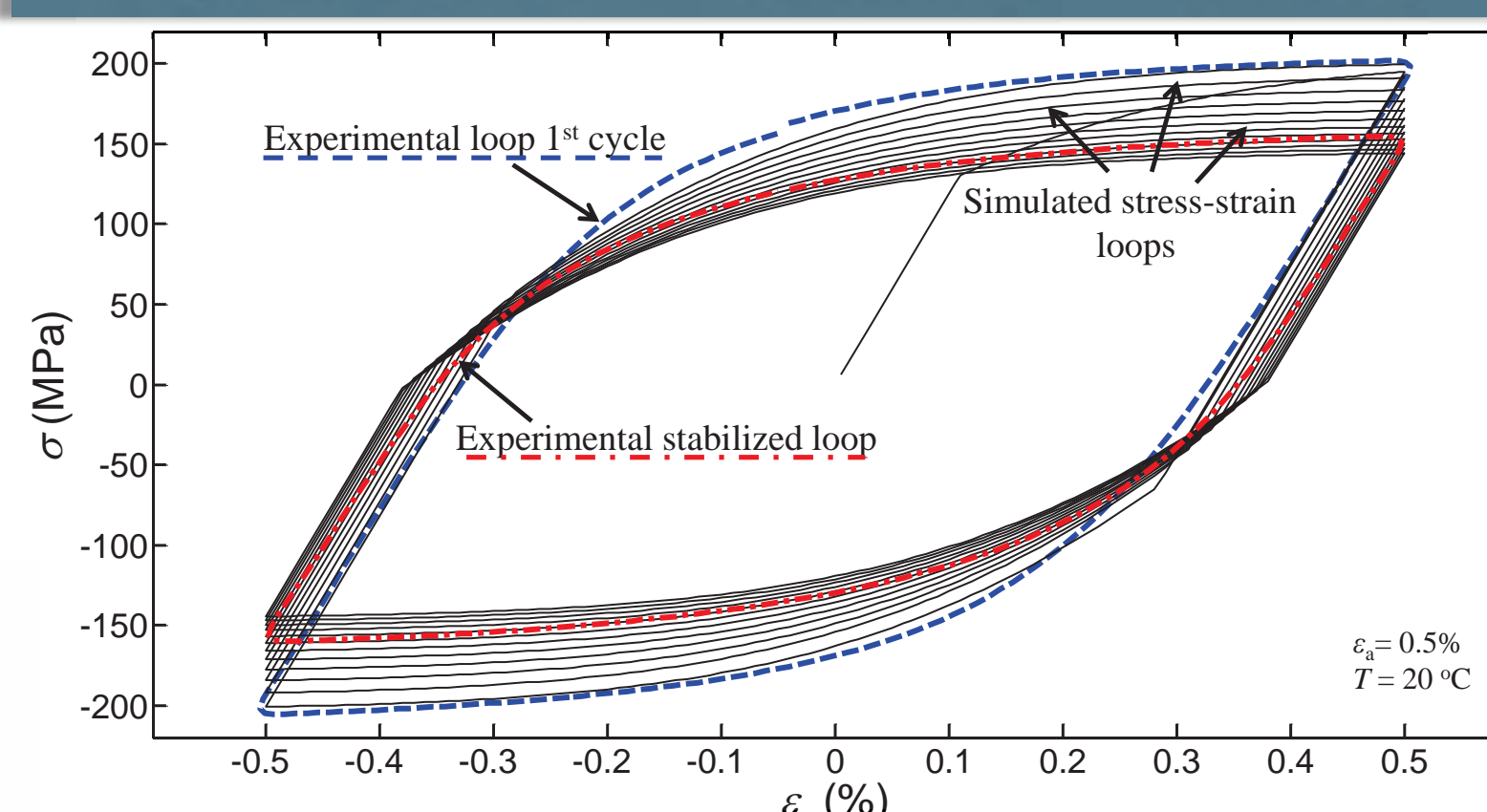
### 2) Parameters identification for nonlinear isotropic model

Estimation of material parameter  $R_\infty$

Estimation of material parameter  $b$



## Experimental vs. simulated stress-strain loops

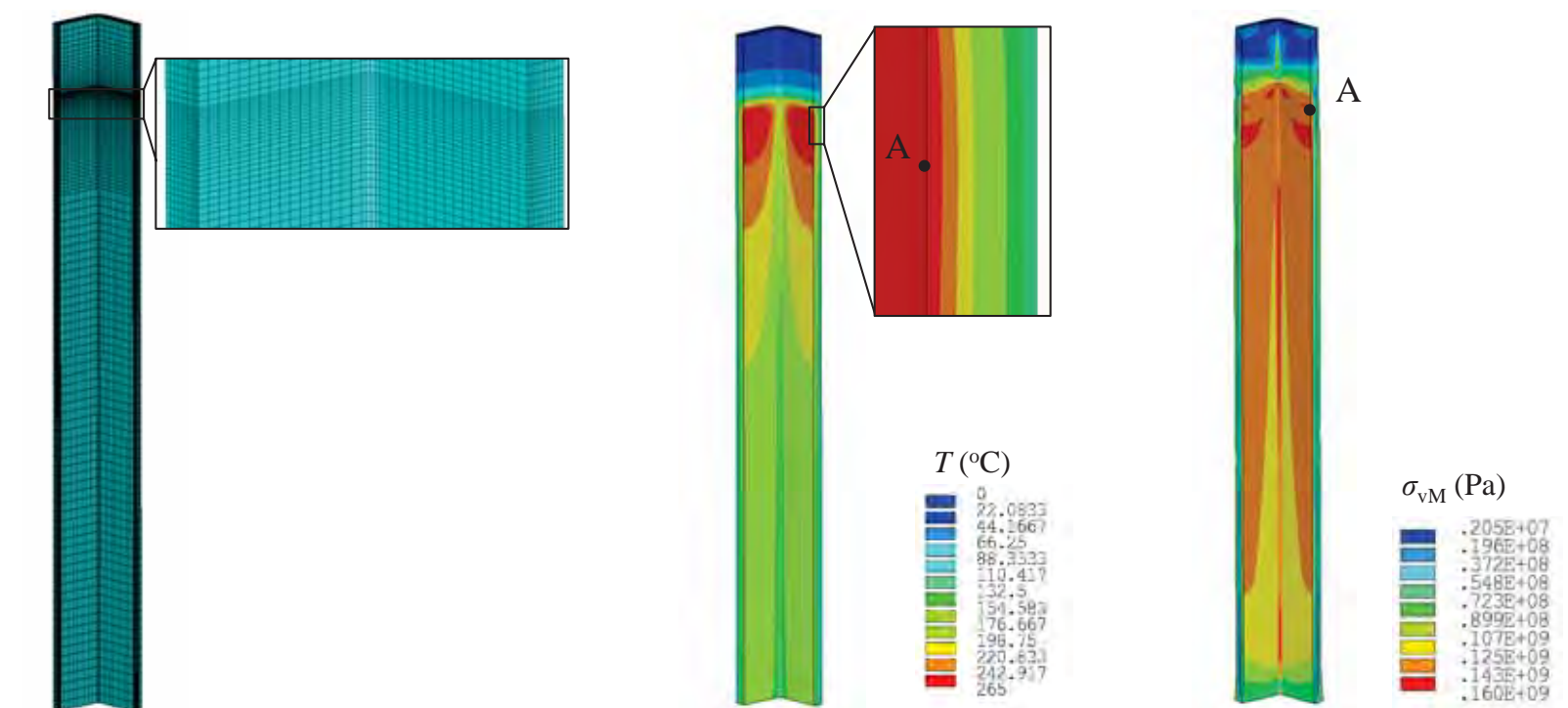


## REFERENCES

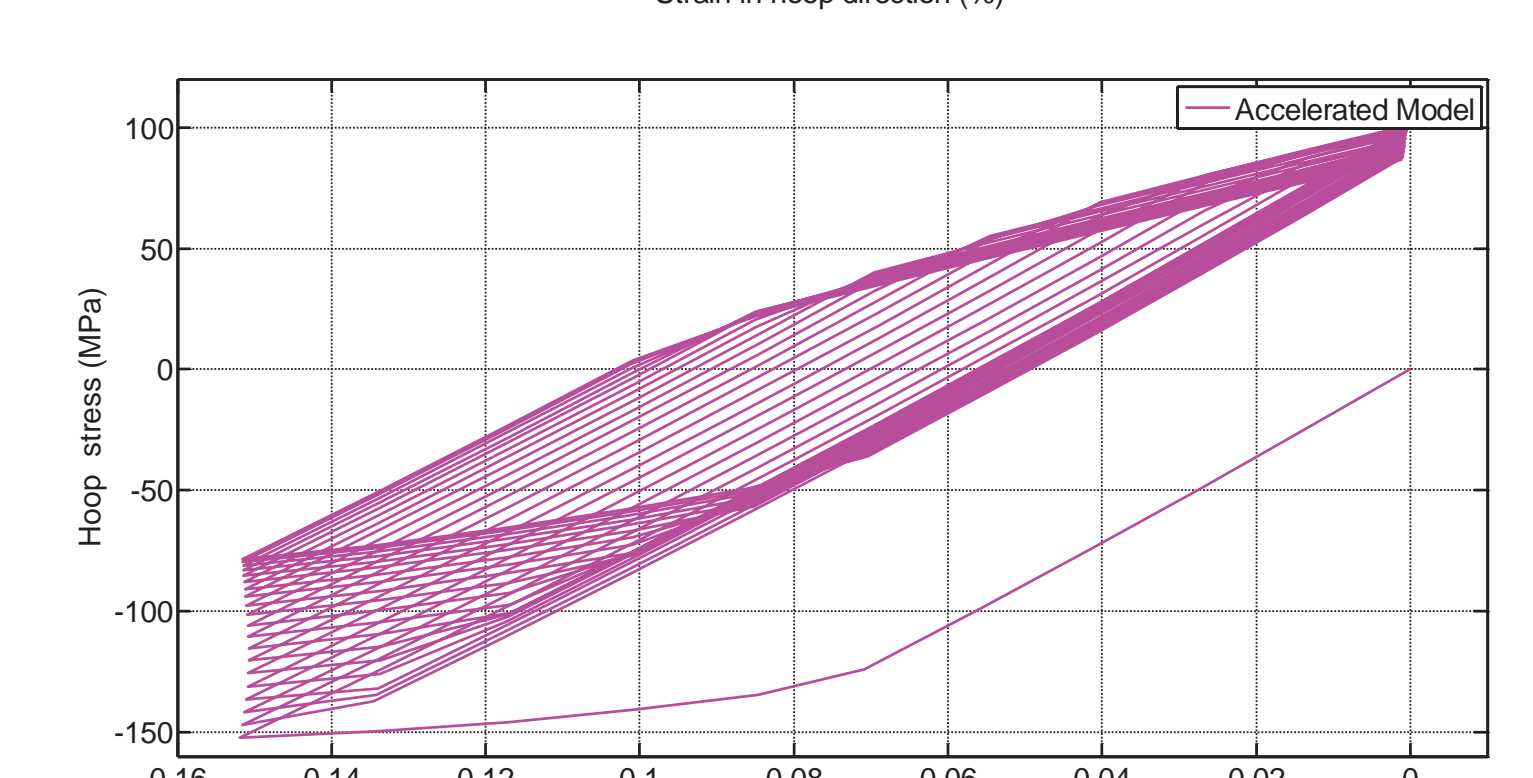
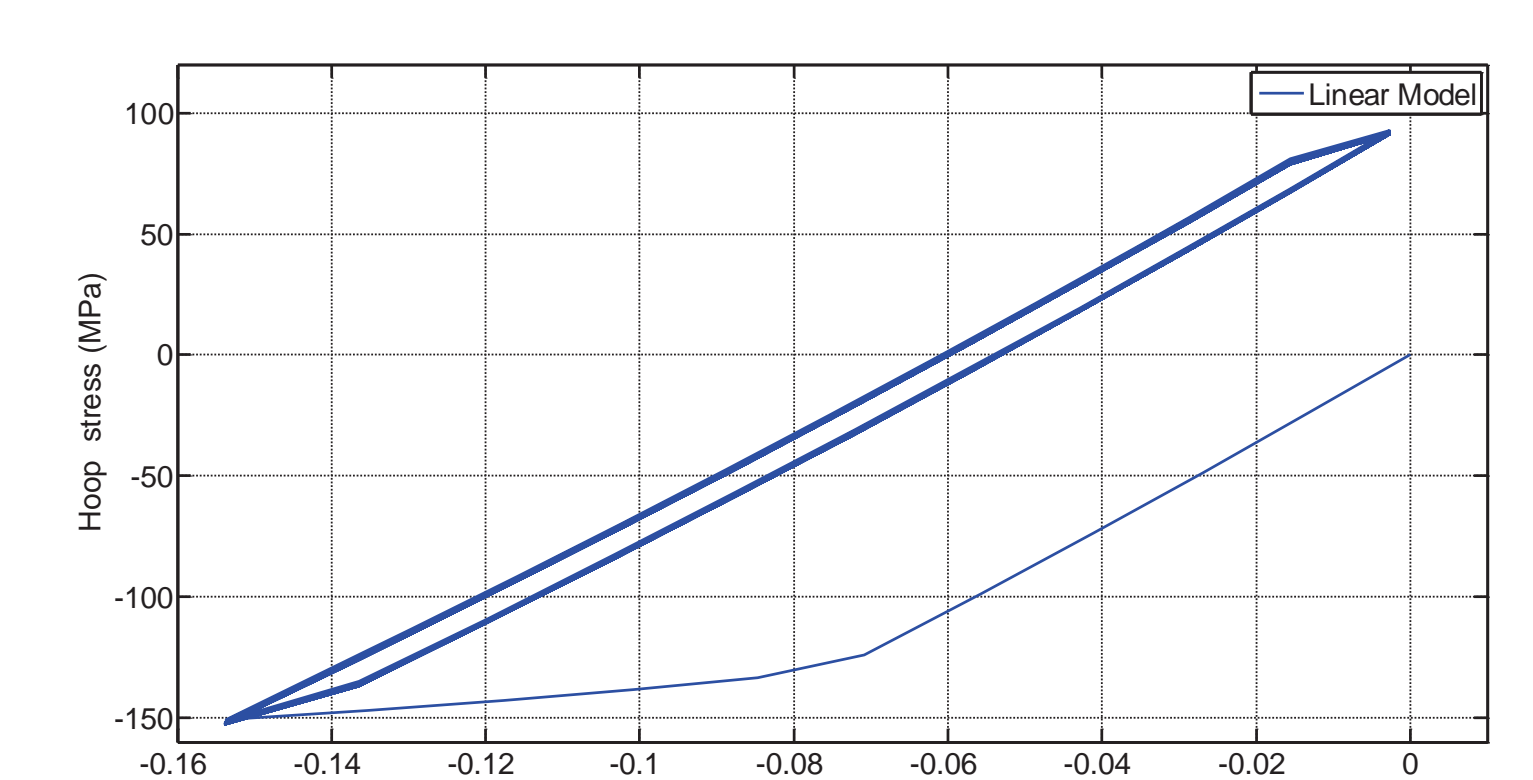
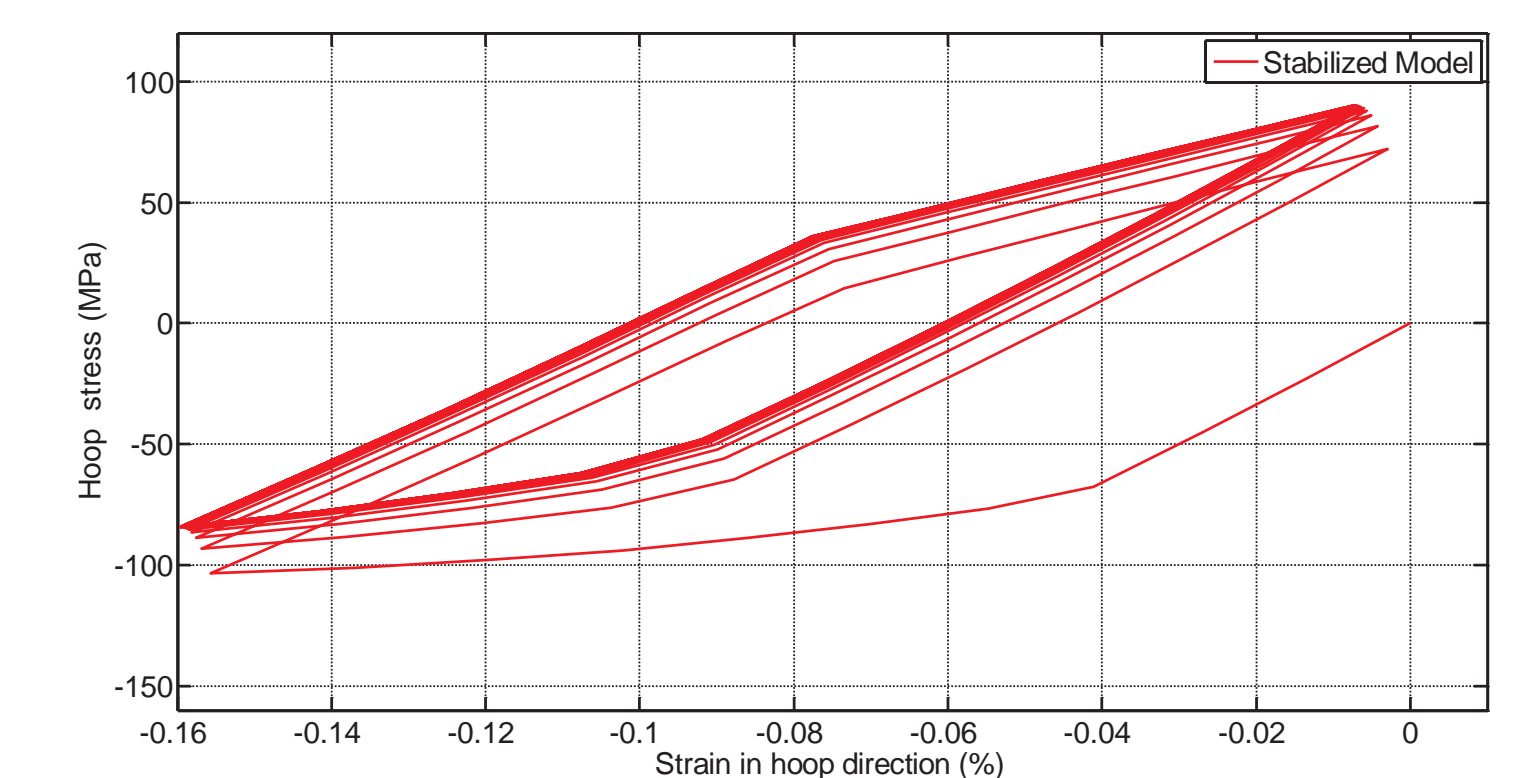
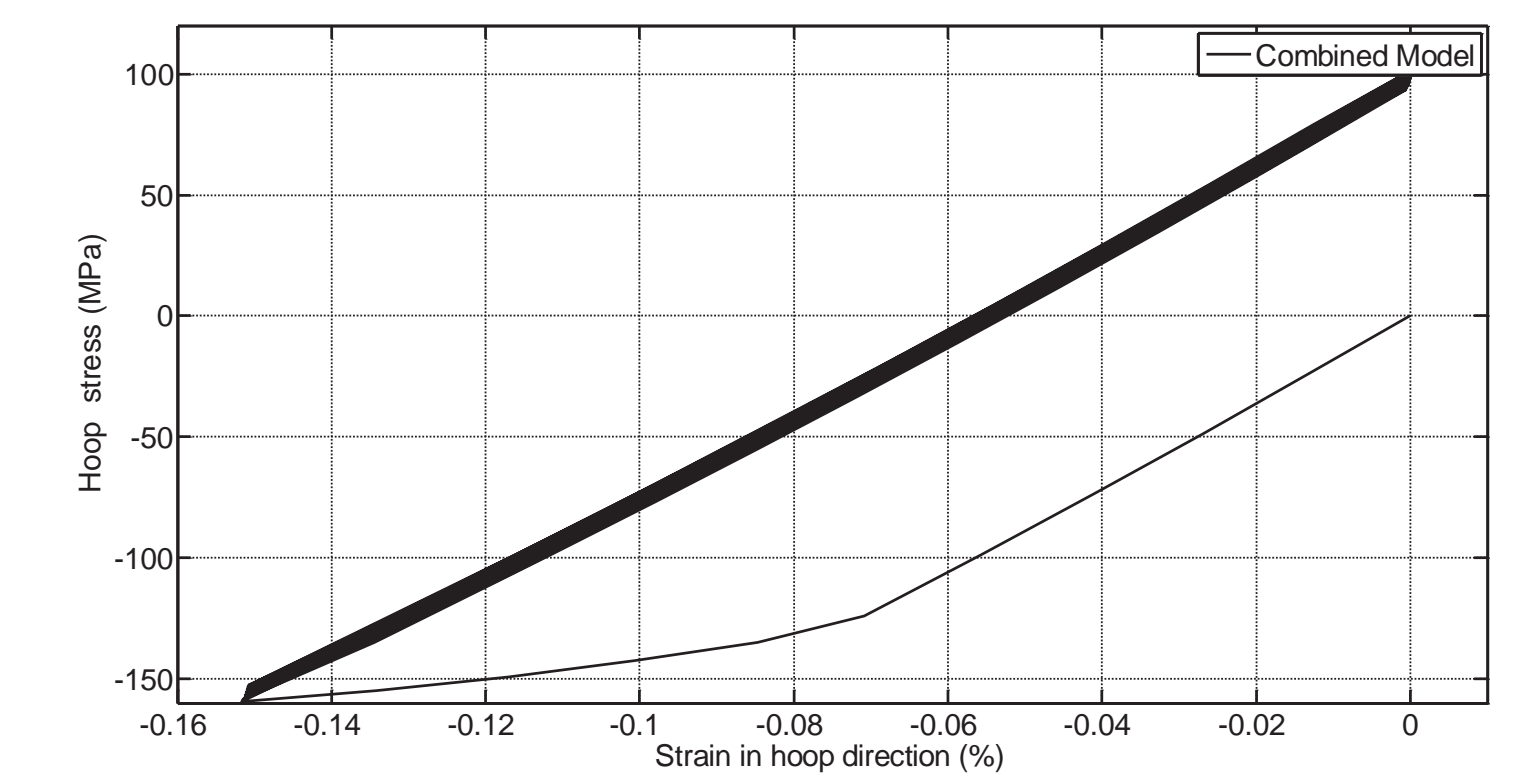
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## Numerical simulation

Temperature and von Mises stress distribution at  $q_{max}$



Evolution of hoop stress-strain for the critical point A in relation with different material models:



## Fatigue life assessment (strain-based approach)

